ELVL-2022-0046469
May 1, 2023

## Orbital Debris Assessment for <br> The M3 CubeSat per NASA-STD 8719.14C

#  Date: 2023.05.02 05:44:38-04'00' 

Mike Perotti, Analyst, NASA KSC VA-H1

 Date: 2023.05.02 09:19:03-04'00'

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National Aeronautics and Space Administration

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Kennedy Space Center, FL 32899


ELVL-2022-0046469
May 1, 2023
Reply to Attn of: VA-H1
TO: Norman Phelps, LSP Mission Manager, NASA/KSC/VA-C
FROM: Mike Perotti, NASA/KSC/VA-H1
SUBJECT: Orbital Debris Assessment Report (ODAR) for the M3 CubeSat
REFERENCES:
A. NASA Procedural Requirements for Limiting Orbital Debris Generation, NPR 8715.6B, 6 February 2017
B. Process for Limiting Orbital Debris, NASA-STD-8719.14C, 05 November 2021
C. International Space Station Reference Trajectory, delivered December 2019
D. McKissock, Barbara, Patricia Loyselle, and Elisa Vogel. Guidelines on Lithiumion Battery Use in Space Applications. Tech. no. RP-08-75. NASA Glenn Research Center Cleveland, Ohio
E. UL Standard for Safety for Lithium Batteries, UL 1642. UL Standard. 5th ed. Northbrook, IL, Underwriters Laboratories, 2012
F. Kwas, Robert. Thermal Analysis of ELaNa-4 CubeSat Batteries, ELVL-20120043254; Nov 2012
G. Range Safety User Requirements Manual Volume 3- Launch Vehicles, Payloads, and Ground Support Systems Requirements, AFSCM 91-710 V3.
H. HQ OSMA Policy Memo/Email to 8719.14: CubeSat Battery Non-Passivation, Suzanne Aleman to Justin Treptow, 10, March 2014
I. ODPO Guidance Email: Fasteners and Screws, John Opiela to Yusef Johnson, 12 February 2020
J. Debris Assessment Software User's Guide: Version 3.1, NASA/TP-2019220300

The intent of this report is to satisfy the orbital debris requirements listed in ref. (a) for the M3 CubeSat launching on the SpaceX Transporter-10 mission. It serves as the final submittal in support of the spacecraft Safety and Mission Success Review (SMSR). Sections 1 through 8 of ref. (b) are addressed in this document; sections 9 through 14 fall under the requirements levied on the primary mission and are not presented here.

This CubeSat will passively reenter, and therefore this ODAR will also serve as the End of Mission Plan (EOMP) for this CubeSat.

| RECORD OF REVISIONS |  |  |
| :---: | :--- | :---: |
| REV | DESCRIPTION | DATE |
| 0 | Original submission | May 2023 |

## Section 1: Program Management and Mission Overview

M3 is sponsored by the Space Operations Mission Directorate at NASA Headquarters. The Program Executive is Michael Rodelo. Responsible program/project manager and senior scientific and management personnel are as follows:

Dr. Hank Pernicka, PM, Missouri Science \& Technology University Joshua Burch, Chief Engineer

The following table summarizes the compliance status of M3, which will be flown on the SpaceX Transporter-10 mission. The current launch date is planned for no earlier than $01 / 24 / 2024$. DAS version 3.2 .3 was used to generate the data provided in this document. M3 is fully compliant with all applicable requirements.

Table 1: Orbital Debris Requirement Compliance Matrix

| Requirement | Compliance Assessment | Comments |
| :--- | :--- | :--- |
| $4.3-1 \mathrm{a}$ | Not applicable | No planned debris release |
| $4.3-1 \mathrm{~b}$ | Not applicable | No planned debris release |
| $4.3-2$ | Not applicable | No planned debris release |
| $4.4-1$ | Compliant | On board energy source <br> (batteries) incapable of <br> debris-producing failure |
| $4.4-2$ | Compliant | On board energy source <br> (batteries) incapable of <br> debris-producing failure |
| $4.4-3$ | Not applicable | No planned breakups |
| $4.4-4$ | Not applicable | No planned breakups |
| $4.5-1$ | Compliant |  |
| $4.5-2$ | Not applicable | Worst case lifetime 13.2 <br> years |
| $4.6-1(\mathrm{a})$ | Compliant |  |
| $4.6-1(\mathrm{~b})$ | Not applicable | Not applicable |
| $4.6-1(\mathrm{c})$ | Not applicable | Passive disposal |
| $4.6-2$ | Not applicable | Not applicable |
| $4.6-3$ | Compliant | Non-credible risk of <br> human casualty |
| $4.6-4$ | Compliant | No planned tether releases |
| $4.6-5$ | Compliant |  |
| $4.7-1$ |  |  |
| $4.8-1$ |  |  |

## Section 2: Spacecraft Description

Table 2 outlines its generic attributes.
Table 2: M3 Attributes

| CubeSat Names | CubeSat <br> Quantity | CubeSat size (mm) | CubeSat <br> Mass <br> (kg) |
| :---: | :---: | :---: | :---: |
| M3 | 1 | $344 \times 108 \times 102$ | 3.54 |

The following pages describe the M3 CubeSat.

## M3 - Missouri University of Science and Technology- 6U



Figure 1: Spacecraft with side panels removed

## Overview

The overall goal of the MMM (Multi-Mode Mission or M3) mission is to demonstrate in the space environment a multi-mode-capable thruster operating in electric mode with a student-developed power processing unit (PPU), utilizing an ionic propellant.

The spacecraft is a single unit with the dimensions of three (3) stacked $10 \mathrm{~cm} \times 10 \mathrm{~cm} \times 10$ cm CubeSat modules (giving an overall dimension of $10 \mathrm{~cm} \times 10 \mathrm{~cm} \times 30 \mathrm{~cm}$.). The total mass is approximately 3.6 kg .

## CONOPS

MMM will be deployed from into $600-\mathrm{km}$ perigee and a $600-\mathrm{km}$ apogee at a $97.61^{\circ}$ inclination. Transmission will begin 45 minutes after deployment and cease after complete battery discharge. Once the propellant reaches the desired temperatures, the flight computer will command the propellant feed system solenoid valves to open and the PPU to supply power to the payload, beginning an electrospray burn. The flight computer will then initiate a burn timer and continue the burn until the burn timer expires or the satellite batteries deplete to $65 \%$ charge. MMM will perform five electric burns for 30 seconds each while in this mode. During the burns, voltage from the payload's extractor will be measured by voltage dividers located on the flight computer and recorded at a rate of 1 Hz for insertion into a multi-mode thruster performance model.

Once the burn timer has expired, MMM will close its solenoid valves, cease measuring the voltage from the voltage dividers, and cease supplying power to the payload. A full system checkout will be performed by the flight computer to ensure the health of MMM. During this time, MMM will also downlink temperature and pressure measurements from the burn and continue regular system health checks. Upon completion of all five burns in Electric Burn Mode, MMM will enter into its Downlink Mode. If, at any point during Electric Burn Mode, the satellite fails a health check, MMM will enter the Primary Safe Mode. Atmospheric drag will quickly decay the orbit until reentry occurs approximately 24 days after launch. No deployables are used. An Eyestar-S3 simplex transmitter is utilized for downlinking thruster test data. An S band receiver on board the satellite can receive a "kill" command to immediately cease all transmissions.

The total delta- $V$ for the mission duration will be $0.05 \mathrm{~m} / \mathrm{s}$. This has a negligible effect to the orbit ( $\sim 0.17 \mathrm{~km}$ worst case).

## Materials

The CubeSat structure is composed of aluminum 6061. It contains standard commercial off-the-shelf (COTS) materials, electrical components, and PCBs with the exception of the in-house developed thruster/propellant feed system (which largely consists of stainless-steel components).

## Hazards

The propulsion system uses an ionic propellant (1-Ethyl-3-methylimidazolium ethyl sulfate $\left(\mathrm{C}_{8} \mathrm{H}_{16} \mathrm{~N}_{2} \mathrm{O}_{4} \mathrm{~S}\right)$ ) classified as "not a hazardous substance or mixture" by its MSDS. The propellant is fed into the thruster by N 2 gas loaded at 30 psia. Inhibits are used to prevent premature pressurant and propellent flow prior to orbit deployment. The electric thruster releases small propellent droplets as part of its nominal operation; at the low orbital altitude and ballistic coefficient of each droplet they are expected to harmlessly disperse very quickly with no chance of presenting a debris hazard (in addition to only having a few ounces of propellant on board). MMM will complete five electric thruster burns lasting 30 seconds. The cubesat will undergo environmental testing with propellant loaded and verify that there are no leaks.


Figure 2: Spacecraft propulsion system CAD


Figure 3: Spacecraft propulsion system schematic

## Batteries

The electrical power storage system consists of four common EaglePicher LCF-133 3.0V Primary D Cell (non-rechargeable) lithium metal batteries with current protection circuitry. The nominal voltage and capacity for each battery is 2.6 V and 16 Ah , respectively. The batteries have a fully welded hermetically sealed design, pressure relief vent, and shutdown separator. A custom battery pack was developed in conjunction with EaglePicher and is assembled in a 4S1P ( 4 series/ 1 parallel) configuration and is protected from reverse current by two active blocking diodes. Each cell is in series with a polymeric positive
temperature coefficient (PTC) device. The PTC is thermally coupled to the cell providing both resettable overload and over-temperature protection. The spacecraft does not have any solar cells. A separate Power Processing Unit (PPU) PCB operates as a transformer, converting the 12 -volt supply into 3400 volts to energize the thruster.

## Section 3: Assessment of Spacecraft Debris Released during Normal Operations

The assessment of spacecraft debris requires the identification of any object ( $>1 \mathrm{~mm}$ ) expected to be released from the spacecraft any time after launch, including object dimensions, mass, and material.

Section 3 requires rationale/necessity for release of each object, time of release of each object, relative to launch time, release velocity of each object with respect to spacecraft, expected orbital parameters (apogee, perigee, and inclination) of each object after release, calculated orbital lifetime of each object, including time spent in Low Earth Orbit (LEO), and an assessment of spacecraft compliance with Requirements 4.3-1 and 4.3-2.

No releases are planned on the M3 CubeSat therefore this section is not applicable.

## Section 4: Assessment of Spacecraft Intentional Breakups and Potential for Explosions.

There are no plans for designed spacecraft breakups, explosions, or intentional collisions for M3.

As discussed in Reference H, with respect to 3U and smaller CubeSats, the probability of battery explosion is very low, and, due to the very small mass of the satellites and their short orbital lifetimes the effect of an explosion on the far-term LEO environment is negligible.

The CubeSat batteries still meet Req. 56450 (4.4-2) by virtue of the HQ OSMA policy regarding CubeSat battery disconnect stating;
"CubeSats as a satellite class need not disconnect their batteries if flown in LEO with orbital lifetimes less than 25 years." (ref. (h))

Limitations in space and mass prevent the inclusion of the necessary resources to disconnect the battery or the solar arrays at EOM. However, the low charges and small battery cells on the CubeSat's power system prevent a catastrophic failure, so that passivation at EOM is not necessary to prevent an explosion or deflagration large enough to release orbital debris.

Assessment of spacecraft compliance with Requirements 4.4-1 through 4.4-4 shows that with a maximum lifetime of 13.2 years maximum, M3 is compliant.

## Section 5: Assessment of Spacecraft Potential for On-Orbit Collisions

Calculation of spacecraft probability of collision with space objects larger than 10 cm in diameter during the orbital lifetime of the spacecraft takes into account both the mean cross sectional area and orbital lifetime.

$$
\text { Mean CSA }=\frac{\sum \text { Surface Area }}{4}=\frac{2 *[(w * l)+(w * h)+(l * h)]}{4}
$$

Equation 1: Mean Cross Sectional Area for Convex Objects

$$
\operatorname{Mean} C S A=\frac{\left(A_{\max }+A_{1}+A_{1}\right)}{2}
$$

Equation 2: Mean Cross Sectional Area for Complex Objects

The CubeSat evaluated for this ODAR is stowed in a convex configuration, indicating there are no elements of the CubeSat obscuring another element of the same CubeSat from view. Thus, the mean CSA for the stowed CubeSat was calculated using
Mean CSA $=\frac{\sum \text { Surface Area }}{4}=\frac{2 *[(w * l)+(w * h)+(l * h)]}{4}$
Equation 1. This configuration renders the longest orbital lifetimes for all CubeSats.
Once a CubeSat has been ejected from the CubeSat dispenser and deployables have been extended, Equation 2 is utilized to determine the mean CSA. $\mathrm{A}_{\text {max }}$ is identified as the view that yields the maximum cross-sectional area. $\mathrm{A}_{1}$ and $\mathrm{A}_{2}$ are the two cross-sectional areas orthogonal to $\mathrm{A}_{\text {max }}$. Refer to Appendix A for component dimensions used in these calculations

M3's assumed orbit at deployment has a $600-\mathrm{km}$ perigee and a $600-\mathrm{km}$ apogee at a $97.61^{\circ}$ inclination which is conservative in that it assumes a high orbit insertion. With an area to mass ratio of $0.0118 \mathrm{~m}^{2} / \mathrm{kg}$, DAS yields 13.2 years for orbit lifetime for its asejected state, which in turn is used to obtain the collision probability. M3 is calculated to have a maximum probability of collision of $4.4 \mathrm{E}-6$. Table 3 below provides complete results.

| CubeSat | м3 |
| :---: | :---: |
| Mass (kg) | 3.541 |


|  | Mean C/S Area (m²) | 0.0416 |
| :---: | :---: | :---: |
|  | Area-to Mass (m²/kg) | 0.0118 |
|  | Orbital Lifetime (yrs) | 13.2 |
|  | Probability of collision ( $10^{-6}$ ) | 4.4 |

Solar Flux Table Dated 12/19/2022
Table 3: CubeSat Orbital Lifetime \& Collision Probability

The probability of M3 colliding with debris or meteoroids greater than 10 cm in diameter that can prevent post-mission disposal is less than 0.00001 , for any configuration. This satisfies the 0.001 maximum probability requirement 4.5-1.

Assessment of spacecraft compliance with Requirements 4.5-1 shows M3 to be compliant.

This ODAR also serves as the EOMP (End of Mission Plan).

## Section 6: Assessment of Spacecraft Post-Mission Disposal Plans and Procedures

M3 will naturally decay from orbit within 25 years after end of the mission, satisfying requirement 4.6-1 a detailing the spacecraft disposal option.

Planning for spacecraft maneuvers to accomplish post-mission disposal is not applicable. Disposal will be achieved via passive atmospheric reentry even if the deorbit device does not deploy.

Calculating the area-to-mass ratio for the worst-case (smallest Area-to-Mass) postmission disposal finds M3 in its stowed configuration as the worst case. The area-to-mass is calculated as follows:

$$
\frac{\operatorname{Mean} C / S \operatorname{Area}\left(m^{2}\right)}{\operatorname{Mass}(\mathrm{kg})}=\operatorname{Area}-\mathrm{to}-\operatorname{Mass}\left(\frac{\mathrm{m}^{2}}{\mathrm{~kg}}\right)
$$

Equation 3: Area to Mass

$$
\frac{0.041628 \mathrm{~m}^{2}}{3.541 \mathrm{~kg}}=0.0118 \frac{\mathrm{~m}^{2}}{\mathrm{~kg}}
$$

The assessment of the spacecraft illustrates it is compliant with Requirements 4.6-1 through 4.6-5.

DAS Orbital Lifetime Calculations:
DAS inputs are: $600-\mathrm{km}$ maximum perigee and $600-\mathrm{km}$ maximum apogee altitudes with an inclination of $97.61^{\circ}$ at deployment no earlier than $01 / 24 / 2024$. An area to mass ratio of $\sim 0.0118 \mathrm{~m}^{2} / \mathrm{kg}$ for the M3 CubeSat was used. DAS yields a 13.2 years orbit lifetime for M3 in its stowed state.

This meets requirement 4.6-1.

## Section 7: Assessment of Spacecraft Reentry Hazards

A detailed assessment of the components to be flown on M3 was performed. The assessment used DAS, a conservative tool used by the NASA Orbital Debris Office to verify Requirement 4.7-1. The analysis is intended to provide a bounding analysis for characterizing the survivability of a CubeSat's component during re-entry. For example, when DAS shows a component surviving reentry, it is not considering the material ablating away or charring due to oxidative heating. Both physical effects are experienced upon reentry and will decrease the mass and size of the real-life components as they reenter the atmosphere, reducing the risk they pose still further.

The following steps are used to identify and evaluate a component's potential reentry risk relative to the 4.7-1 requirement of having less than 15 J of kinetic energy and a $1: 10,000$ probability of a human casualty in the event it survives reentry.

1. Low melting temperature (less than $1000^{\circ} \mathrm{C}$ ) components are identified as materials that would never survive reentry and pose no risk of human casualty. This is confirmed through DAS analysis that showed materials with melting temperatures equal to or below that of copper $\left(1080^{\circ} \mathrm{C}\right)$ will always demise upon reentry for any size component up to the dimensions of a 1 U CubeSat.
2. The remaining high temperature materials are shown to pose negligible risk of human casualty through a bounding DAS analysis of the highest temperature components, stainless steel $\left(1500^{\circ} \mathrm{C}\right)$. If a component has a melting temperature between $1000^{\circ} \mathrm{C}$ and $1500^{\circ} \mathrm{C}$, it can be expected to possess the same negligible risk as a stainless steel component of similar dimensions.
3. Fasteners and similar materials that are composed of stainless steel or a lower melting point material will not be input into DAS, as suggested by guidance from the Orbital Debris Project Office (Reference I)

Table 4: M3 High Melting Temperature Material Analysis

| Name | Material | Total Mass (kg) | Demise <br> Alt (km) | Kinetic <br> Energy (J) |
| :---: | :---: | :---: | :---: | :---: |
| Pressurant Tank | AISI 316 Stainless <br> Steel | 0.1450 | 74.8 | - |
| Battery D-Cell | Stainless <br> Steel/Lithium | 0.3415 | 73.3 | - |
| $1 / 2^{\prime \prime}$ to 1/8" Union <br> Reducer | Stainless Steel | 0.0780 | 72.3 | - |
| 1/8" Check Valve | Stainless Steel 316 | 0.2978 | 73.6 | - |
| $1 / 2 " ~ t o ~ 1 / 4 " ~ S t e m ~$ <br> Reducer | AISI 316 Stainless <br> Steel | 0.0659 | 74.0 | - |
| $1 / 4$ ", 1/8" Tee Fitting | AISI 316 Stainless <br> Steel | 0.0599 | 76.9 | - |
| 3/8" to 1/8" Union <br> Reducer | AISI 316 Stainless <br> Steel | 0.0419 | 74.6 | - |
| 1/8" Tee Fitting | Stainless Steel 316 | 0.1254 | 75.6 | - |
| Pressure Transducer | Stainless Steel 316 | 0.0720 | 74 | - |
| Thruster Heatsink | AISI 316 Stainless <br> Steel | 0.0300 | 75.7 | - |
| 1/8" Elbow | Stainless Steel 316 | 0.0596 | 75.5 | - |


| Name | Material | Total Mass (kg) | Demise Alt (km) | Kinetic Energy (J) |
| :---: | :---: | :---: | :---: | :---: |
| 1/4" Tube | AISI 316 Stainless Steel | 0.0270 | 75.8 | - |
| 1/2" diam Propellant Tank | Stainless Steel 316 | 0.0215 | 76.6 | - |
| 1/4" 10-32 Male SAE | AISI 316 Stainless Steel | 0.0206 | 75.5 | - |
| Extractor Grid | AISI 316 Stainless Steel | 0.0199 | 76 | - |
| Union 1/8" to 1/16" | Stainless Steel 316 | 0.0177 | 75.4 | - |
| $\begin{gathered} \hline 1 / 8^{\prime \prime} \text { to } 1 / 16^{\text {" }} \text { Union } \\ \text { Reducer } \end{gathered}$ | Stainless Steel 316 | 0.0177 | 75.4 | - |
| 1/16" Elbow | Stainless Steel 316 | 0.0163 | 75.9 | - |
| 1/8" 10-32 Male SAE | AISI 316 Stainless Steel | 0.0134 | 75.9 | - |
| 10-32 Female Adapter | AISI 316 Stainless Steel | 0.0194 | 75.6 | - |
| Hysteresis Rod | Nickel | 0.0246 | 76.6 | - |
| $\begin{gathered} \hline 1 / 16^{\prime \prime} \text { to } 1 / 8 " \text { Stem } \\ \text { Adapter } \\ \hline \end{gathered}$ | AISI 316 Stainless Steel | 0.0059 | 76.8 | - |
| Solenoid Valve | 316 Stainless Steel Chrome Core 18 | 0.0227 | 77.1 | - |
| 1/8" 90deg Connector | AISI 316 Stainless Steel | 0.0045 | 77.1 | - |
| 1/8" 180 deg Tube | AISI 316 Stainless Steel | 0.0084 | 77.2 | - |
| 1/8" Prop to Thruster Pipe | AISI 316 Stainless Steel | 0.0035 | 77.3 | - |
| 1/8" Tube | AISI 316 Stainless Steel | 0.0022 | 77.3 | - |
| 1/8" Connector Tube | Stainless Steel 316 | 0.0019 | 77.4 | - |
| 1/8" Tube | AISI 316 Stainless Steel | 0.0018 | 77.3 | - |
| 1/8" Connector Tube | AISI 316 Stainless Steel | 0.0015 | 77.3 | - |
| 1/8" Connector Tube | Stainless Steel 316 | 0.0036 | 77.3 | - |
| $\begin{gathered} \hline 1 / 8^{\prime \prime} \text { to } 1 / 16^{\prime \prime} \text { Port } \\ \text { Connector } \end{gathered}$ | AISI 316 Stainless Steel | 0.0012 | 77.5 | - |
| 1/8" to 1/16" Port <br> Reducing | AISI 316 Stainless Steel | 0.0012 | 77.5 | - |

All high melting point components demise upon reentry and M3 complies with the $1: 10,000$ probability of Human Casualty Requirement 4.7-1. A breakdown of the determined probabilities follows:

Table 5: Requirement 4.7-1 Compliance by CubeSat

| Name | Status | Risk of Human <br> Casualty |
| :---: | :---: | :---: |
| M3 | Compliant | $1: 100,000,000$ |

*Requirement 4.7-1 Probability of Human Casualty $\leq 1: 10,000$
If a component survives to the ground but has less than 15 Joules of kinetic energy, it is not included in the Debris Casualty Area that inputs into the Probability of Human Casualty calculation. M3 has a $1: 100,000,000$ probability, as none of its components survive.

M3 is compliant with Requirement 4.7-1 of NASA-STD-8719.14C.

## Section 8: Assessment for Tether Missions

M3 will not be deploying any tethers.

## Section 9-14

ODAR sections 9 through 14 pertain to the launch vehicle, and are not covered here. Launch vehicle sections of the ODAR are the responsibility of the launch provider.

If you have any questions, please contact the undersigned at 321-205-4667.
/original signed by/
Mike Perotti
Flight Design Analyst NASA/KSC/VA-H1
cc : VA-C/Liam J. Cheney
VA-C/Norman L. Phelps AIS2/ Jennifer A. Snyder SA-D1/Kevin R. Villa
SA-D2/Homero Hidalgo

## Appendix Index:

Appendix A. M3 Component List
M3 Component List
Appendix A．

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|  | $\begin{aligned} & \stackrel{\rightharpoonup}{0} \\ & \underset{0}{2} \end{aligned}$ | $\begin{aligned} & \infty \\ & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { Bi } \\ & \text { in } \end{aligned}$ |  | $\begin{aligned} & \tilde{q} \\ & \underset{\sim}{\dot{q}} \end{aligned}$ | $\begin{gathered} \underset{\sim}{\underset{A}{n}} \\ \underset{\sim}{n} \end{gathered}$ | $\frac{\underset{\lambda}{\lambda}}{\underset{\sim}{n}}$ | $\begin{aligned} & \mathrm{B} \\ & \stackrel{y}{2} \end{aligned}$ | $\begin{gathered} \text { F } \\ \stackrel{\rightharpoonup}{\circ} \end{gathered}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{c} \\ & \stackrel{1}{i} \end{aligned}$ | $\begin{aligned} & \mathrm{g} \\ & \dot{\sim} \\ & \dot{n} \end{aligned}$ | $\begin{aligned} & \bar{\infty} \\ & \dot{\infty} \\ & \dot{\alpha} \end{aligned}$ |  |  |  |  | $\begin{aligned} & \stackrel{8}{0} \\ & \stackrel{0}{2} \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 . \\ & \hline 0 \end{aligned}$ |  | $\begin{aligned} & \stackrel{\otimes}{\circ} \\ & = \end{aligned}$ | $\begin{aligned} & \underset{\sim}{q} \\ & \infty \end{aligned}$ | $\begin{aligned} & 0 \\ & \stackrel{0}{+} \\ & \underset{N}{2} \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 . \\ & \hline-1 \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \underset{\sim}{i} \end{aligned}$ |  |
| 镸会 | $\begin{gathered} \underset{\sim}{2} \\ \underset{子}{子} \\ \stackrel{n}{2} \end{gathered}$ | $\begin{gathered} \underset{\sim}{\underset{~}{2}} \\ \underset{\sim}{子} \end{gathered}$ | $\begin{aligned} & 8 \\ & \hline 8 \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \mathrm{O} \\ & \hline \mathrm{O} \\ & \mathrm{c} \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \hline \mathrm{O} \\ & \mathrm{o} \\ & \hline \end{aligned}$ | $\begin{aligned} & 8.8 \\ & \hline \text { r } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \hline \mathrm{O} \\ & \mathrm{o} \\ & \hline \end{aligned}$ | 8 <br> 8 |  | $\begin{aligned} & \mathrm{O} \\ & \hline \mathrm{O} \\ & \mathrm{o} \\ & \text { n } \end{aligned}$ | $\begin{aligned} & 8 \\ & \hline 8 \\ & \text { ri } \end{aligned}$ |  |  |  |  | $\begin{aligned} & \text { ob } \\ & \hline \mathbf{o} \end{aligned}$ | $$ | $$ | $\begin{aligned} & \bar{N} \\ & \stackrel{\rightharpoonup}{n} \end{aligned}$ | $\frac{\square}{3}$ | $\begin{aligned} & 8 \\ & \hline 8 \\ & \hline \\ & \hline \end{aligned}$ | 8 <br> 8 <br> 8 | $$ | － |
|  |  | $\begin{gathered} \underset{\sim}{\underset{~}{2}} \\ \underset{\sim}{子} \end{gathered}$ | $\begin{aligned} & \mathrm{O} \\ & \underset{\mathrm{O}}{ } \end{aligned}$ |  | $\begin{aligned} & \text { N} \\ & \text { 人 } \\ & \text { 人 } \end{aligned}$ | $\begin{aligned} & 8 \\ & \hline 8 \\ & \dot{0} \\ & \hline \end{aligned}$ | $\begin{gathered} \underset{0}{0} \\ \underset{\sim}{\mathrm{i}} \end{gathered}$ | $\begin{aligned} & \circ \\ & \hline 0 \\ & \hline- \end{aligned}$ | $\begin{aligned} & n \\ & \infty \\ & \underset{\sim}{\infty} \end{aligned}$ | $\begin{aligned} & \underset{\sim}{\infty} \\ & \infty \\ & \infty \end{aligned}$ | $\begin{aligned} & \mathrm{o} \\ & \stackrel{8}{\mathrm{n}} \end{aligned}$ | $\begin{aligned} & \dot{+} \\ & \stackrel{\infty}{\dot{\omega}} \end{aligned}$ |  |  |  |  | $\begin{aligned} & \text { d } \\ & \underset{A}{\lambda} \end{aligned}$ | $\begin{gathered} n \\ n \\ n \\ n \\ \text { n } \end{gathered}$ | $\begin{aligned} & \overrightarrow{\underset{G}{子}} \\ & \dot{\sim} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{\infty}{1} \\ & = \end{aligned}$ | $\begin{aligned} & \frac{\pi}{6} \\ & \frac{1}{9} \end{aligned}$ | $\begin{aligned} & \dot{m} \\ & \underset{m}{m} \end{aligned}$ | $\begin{aligned} & n \\ & \hat{n} \\ & n \\ & n \end{aligned}$ | $\begin{aligned} & \stackrel{0}{\infty} \\ & \stackrel{\infty}{\leftrightharpoons} \end{aligned}$ | \％ |
| 号 | $c_{\infty}^{\infty}$ | $\begin{aligned} & \circ \\ & \vdots \\ & 0 \\ & \text { co } \end{aligned}$ | $\begin{aligned} & \text { 정 } \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \pm \\ & \underset{\sim}{\top} \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & \bar{\sim} \\ & \underset{\substack{2}}{ } \end{aligned}$ |  | $\begin{aligned} & \overline{6} \\ & \stackrel{0}{0} \end{aligned}$ | $\begin{aligned} & \infty \\ & \infty \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { ob } \\ & \text { d } \\ & \mathbf{O} \end{aligned}$ | $\begin{aligned} & \text { n } \\ & \text { in } \\ & 0 \end{aligned}$ |  | $\begin{aligned} & \text { a } \\ & \text { n } \\ & \end{aligned}$ | $\begin{aligned} & \text { N} \\ & \text { N} \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \hline 0 \\ & \hline- \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { I } \\ & \substack{\infty \\ \text { d }} \end{aligned}$ |  | $\begin{aligned} & \text { K } \\ & \text { 子 } \\ & \text { d } \end{aligned}$ | $\begin{gathered} \underset{\sim}{n} \\ \underset{\sim}{\omega} \end{gathered}$ | $\begin{aligned} & \stackrel{\leftrightarrow}{甘} \\ & \stackrel{\Delta}{6} \end{aligned}$ | $\begin{aligned} & \text { ৪i } \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & \text { ৪} \\ & \stackrel{\circ}{7} \end{aligned}$ | $\begin{aligned} & \text { ô } \\ & \text { O} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \underset{O}{O} \\ & \underset{ذ}{ذ} \end{aligned}$ | $\begin{aligned} & \stackrel{\imath}{6} \\ & \underset{O}{a} \\ & \end{aligned}$ | $n cn$ |
|  |  |  | $\begin{array}{\|l\|l} \hline \stackrel{y}{\approx} \\ \hline \end{array}$ | $\frac{\stackrel{y}{0}}{2}$ | $\begin{array}{\|c} \stackrel{y}{\leftrightarrows} \\ \end{array}$ |  | $\begin{array}{\|c} \stackrel{\cong}{2} \\ \hline \end{array}$ |  | $\begin{array}{\|c} \frac{2}{5} \\ \frac{\pi}{2} \end{array}$ | $\begin{array}{\|c} \stackrel{0}{2} \\ \hline \end{array}$ | $\begin{aligned} & \text { 気 } \\ & \stackrel{F}{E} \\ & \vec{d} \end{aligned}$ | $\begin{array}{\|l} \stackrel{0}{\pi} \\ \stackrel{y}{\pi} \end{array}$ |  |  |  |  |  | $\begin{array}{\|c} \stackrel{0}{\Xi} \\ \end{array}$ | $\stackrel{\stackrel{y}{\pi}}{\stackrel{\pi}{\approx}}$ |  | $\begin{aligned} & \stackrel{\rightharpoonup}{0} \\ & \stackrel{B}{B} \\ & \hline 0 \end{aligned}$ | $\begin{array}{\|c} \stackrel{y}{5} \\ \hline \end{array}$ | $\begin{array}{\|c} \stackrel{0}{\pi} \\ \end{array}$ | $\begin{array}{\|l\|} \hline \frac{\pi}{2} \\ \hline \end{array}$ | $\stackrel{\text { \％}}{\sim}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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|  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \underset{J}{J} \\ & \frac{\rightharpoonup}{d} \\ & \tilde{d} \end{aligned}$ | $\begin{array}{\|l\|l} n \\ \stackrel{\rightharpoonup}{u} \\ \stackrel{\rightharpoonup}{u} \\ 0 \end{array}$ | $\begin{aligned} & \mathrm{N} \\ & \stackrel{\rightharpoonup}{\mathrm{v}} \\ & \underset{\sim}{v} \end{aligned}$ |  |  |  |  |  |  |  |  |  | ك |
| 高 | F | $\stackrel{\sim}{\square}$ | ヲ | in | in | in | in | 示 | in | in | in | $\stackrel{\sim}{\sim}$ | is | 8 | $\bar{\square}$ | T | $\bigcirc$ | d | \％ | \％ | ¢ | $\stackrel{\circ}{\circ}$ | 8 | $\stackrel{\square}{2}$ | ス |


|  | $\begin{aligned} & \stackrel{0}{0} \\ & \stackrel{y}{0} \\ & 0 \end{aligned}$ |  |  |  | $\begin{aligned} & \stackrel{.0 .0}{0} \\ & \stackrel{y}{0} \end{aligned}$ | $\begin{aligned} & 0.0 \\ & \stackrel{0}{\overline{0}} \\ & \stackrel{0}{0} \end{aligned}$ |  |  |  |  | $\begin{aligned} & \stackrel{0}{0} \\ & \stackrel{0}{0} \\ & \stackrel{0}{0} \end{aligned}$ | $\begin{aligned} & 0.0 \\ & \stackrel{0}{0} \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \stackrel{0}{0} \\ & \stackrel{0}{0} \\ & 0 \end{aligned}$ |  | $\left\|\begin{array}{c} \stackrel{0}{0} \\ \ddot{g} \\ \stackrel{0}{0} \end{array}\right\|$ |  | $\begin{aligned} & \stackrel{0}{0} \\ & \stackrel{0}{0} \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & \stackrel{0}{0} \\ & \stackrel{0}{0} \\ & \hline 0 . \end{aligned}$ | $\begin{gathered} \stackrel{0}{0} \\ \stackrel{y}{0} \\ \stackrel{0}{0} \end{gathered}$ | $\begin{aligned} & 0.0 \\ & 0 \\ & 0 \end{aligned}$ |  | $\begin{aligned} & \stackrel{0}{0} \\ & \stackrel{0}{0} \\ & \hline 0 . \end{aligned}$ | $\begin{gathered} \stackrel{0}{0} \\ \stackrel{y}{0} \\ 0 \end{gathered}$ | － |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
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|  | $\stackrel{\circ}{2}$ | 2 | $\%^{\circ}$ | \％ | \％ | 2 | $\stackrel{\circ}{2}$ | \％ | \％ | \％ | $\bigcirc$ | \％ | \％ | $\stackrel{\bullet}{\bullet}$ | \％ | \％ | \％ | \％ | \％ | \％ | \％ | \％ | $\stackrel{\circ}{2}$ | \％ |
|  | $\begin{aligned} & \tilde{G} \\ & \dot{G} \end{aligned}$ |  | $\begin{aligned} & \underset{\sim}{\alpha} \\ & \underset{子}{2} \end{aligned}$ | $\begin{aligned} & \infty \\ & \substack{\infty \\ 0 \\ 0 \\ \hline} \end{aligned}$ | $\begin{aligned} & 9 \\ & 7 \\ & \dot{q} \end{aligned}$ | $\begin{aligned} & n \\ & n \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{gathered} n \\ n \\ 0 \\ 0 \end{gathered}$ | $\begin{aligned} & 8 \\ & \hline- \\ & \hline- \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{8} \\ & \hline \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{\circ}{0} \end{aligned}$ | $\begin{aligned} & \infty \\ & \infty \\ & 0 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & i n \\ & n \\ & \dot{m} \end{aligned}$ | $\begin{aligned} & 0 \\ & n \\ & 0 \\ & j \\ & \hline \end{aligned}$ | $\begin{gathered} \text { Ǹ } \\ \text { O} \end{gathered}$ | $\begin{aligned} & \infty \\ & \infty \\ & 0 \\ & \underset{j}{2} \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \underset{y}{q} \end{aligned}$ | $\begin{gathered} \text { ત̀ } \\ \text { ત̀n } \end{gathered}$ | $\begin{aligned} & \stackrel{0}{\infty} \\ & \stackrel{\rightharpoonup}{\dot{~}} \end{aligned}$ | $\begin{aligned} & \tilde{N} \\ & \vdots \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { ơ } \\ & \stackrel{y}{6} \\ & \hline-1 \end{aligned}$ | $\stackrel{\underset{N}{*}}{\stackrel{H}{m}}$ | $\frac{\pi}{2}$ | $\begin{aligned} & \mathrm{g} \\ & \text { i } \\ & \text { in } \end{aligned}$ |  |
|  | $\begin{aligned} & 8 \\ & \hline 8 \\ & 0 \\ & 0 \end{aligned}$ |  | $\begin{aligned} & \underset{\sim}{4} \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & \stackrel{8}{0} \\ & \stackrel{\rightharpoonup}{+} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \hline 8 \\ & \mathrm{o} \end{aligned}$ | $\begin{aligned} & 8 \\ & \hline 8 \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \hline \mathrm{O} \\ & \hline \end{aligned}$ | $\begin{aligned} & 8 \\ & \dot{8} \\ & \dot{1} \end{aligned}$ | $\begin{aligned} & \stackrel{8}{8} \\ & \stackrel{\rightharpoonup}{i} \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { in } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & \\ & \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{n} \\ & = \end{aligned}$ | $\stackrel{\circ}{\underset{m}{n}}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\dot{G}} \\ & \underset{j}{2} \end{aligned}$ |  | $\stackrel{\infty}{\stackrel{\infty}{¿}}$ | $\begin{aligned} & \text { 8} \\ & \text { O} \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N} \\ & \text { cin } \end{aligned}$ | $\begin{gathered} \text { 寸 } \\ \text { d } \end{gathered}$ | $\frac{8}{0}$ | $\stackrel{\ddots}{7}$ | $\begin{aligned} & \underset{\substack{8 \\ \hline \\ 0}}{ } \end{aligned}$ | $\stackrel{\square}{\circ}$ |
|  | $\begin{aligned} & 8 \\ & \hline 0 \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \text { 芯 } \\ & \stackrel{\text { Nu}}{ } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \stackrel{\rightharpoonup}{\dot{n}} \\ & \dot{N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \stackrel{8}{\mathrm{o}} \\ & \text {. } \end{aligned}$ | $\begin{gathered} \underset{\infty}{8} \\ \underset{\infty}{\circ} \\ \hline \end{gathered}$ |  | $\begin{gathered} 8 \\ \hline 0 \\ \infty \\ \infty \\ \hline \end{gathered}$ | $\begin{aligned} & 8 \\ & \hline 8 \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 . \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & \infty \\ & \underset{\sim}{m} \\ & \hline \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 . \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & \hline 8 \end{aligned}$ | $\stackrel{i n}{\underset{m}{m}}$ | $\begin{gathered} \overrightarrow{7} \\ \stackrel{y}{6} \end{gathered}$ | $\begin{aligned} & \text { Z } \\ & \underset{\sim}{n} \end{aligned}$ | $\stackrel{\infty}{\stackrel{\infty}{¿}}$ |  | $\begin{aligned} & \text { O} \\ & \text { H} \\ & \text { çin } \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{0}{4} \\ & \dot{4} \end{aligned}$ | $\frac{8}{6}$ | $\stackrel{i}{n}$ | $\begin{aligned} & \underset{\sim}{8} \\ & \underset{\sim}{0} \\ & \hline \end{aligned}$ | ¢ |
| $\Sigma_{0}^{\circ} \text { o }$ | $\begin{gathered} \pm \\ \underset{\sim}{\lambda} \end{gathered}$ | $\begin{aligned} & \text { n } \\ & \dot{\sim} \\ & \dot{\sim} \end{aligned}$ | $\begin{gathered} \text { N} \\ \text { Ǹ } \end{gathered}$ | $\begin{aligned} & \infty \\ & \infty \\ & \stackrel{\infty}{\infty} \end{aligned}$ | $\begin{aligned} & \text { なे } \\ & \text { ci } \end{aligned}$ | $\frac{i n}{6}$ | $\begin{gathered} \text { Oin } \\ \text { Nín } \end{gathered}$ | $\begin{aligned} & \bar{\infty} \\ & \infty \\ & \infty \\ & \infty \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 6 \end{aligned}$ | $\underset{\underset{\sim}{\infty}}{\stackrel{\otimes}{\infty}}$ | $\begin{aligned} & \stackrel{Q}{Q} \\ & \underset{I}{2} \end{aligned}$ | $$ | $\begin{aligned} & \underset{8}{8} \\ & \stackrel{0}{\infty} \end{aligned}$ | $\underset{\sim}{\underset{\sim}{n}}$ | $\left.\begin{gathered} \underset{\sim}{c} \\ \underset{\sim}{n} \end{gathered} \right\rvert\,$ | $\underset{\infty}{\stackrel{t}{\circ}}$ | $\begin{aligned} & \text { oi} \\ & \underset{6}{\circ} \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{\circ}{\overleftarrow{O}} \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & \text { Oin } \\ & \text { O} \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & \text { ty } \\ & \text { © } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline 0.0 \\ & \hline . \end{aligned}$ | $\begin{gathered} \stackrel{\circ}{\mathrm{N}} \\ \underset{\sim}{*} \end{gathered}$ | $\begin{aligned} & \stackrel{\ddots}{6} \\ & \stackrel{\rightharpoonup}{\ominus} \end{aligned}$ |  |
|  | $\begin{aligned} & \stackrel{0}{\pi} \\ & \frac{\pi}{2} \end{aligned}$ | 㿫 |  | $\begin{array}{\|l\|} \hline \frac{\pi}{2} \\ \hline \end{array}$ | $\frac{\stackrel{y}{0}}{2}$ |  | $\begin{array}{\|l\|l} \hline \stackrel{y}{5} \\ \hline \end{array}$ | $\frac{\stackrel{y}{\leftrightarrows}}{\stackrel{y}{\sim}}$ | $\begin{array}{\|c} \stackrel{y}{5} \\ \stackrel{y}{\circ} \end{array}$ | $\begin{array}{\|l} \stackrel{0}{\pi} \\ \stackrel{y}{\pi} \end{array}$ | $\stackrel{\star}{\circ}$ | $\begin{array}{\|c} \stackrel{y}{\leftrightarrows} \\ \stackrel{y}{\sim} \end{array}$ |  |  | $\frac{\stackrel{y}{0}}{a}$ | $\begin{aligned} & \text { 気 } \\ & \text { 旡 } \end{aligned}$ |  | $\frac{\stackrel{y}{\pi}}{2}$ |  | $\frac{\cong}{\vdots}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{t} \\ & \stackrel{y}{B} \\ & \widehat{X} \end{aligned}$ |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \stackrel{\rightharpoonup}{0} \\ & \stackrel{0}{0} \\ & \hline 0 \end{aligned}$ |  |  |  | $\begin{array}{\|l} 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{array}$ |  |
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|  |  |  |  |  |  | $\begin{aligned} & \mathbb{1} \\ & \overrightarrow{0} \\ & \stackrel{0}{0} \\ & \vec{i} \\ & \stackrel{0}{i n} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \frac{\pi}{0} \\ & \text { in } \\ & 0 \\ & \infty \\ & \infty \\ & \dot{\infty} \end{aligned}$ |  |  | $\begin{aligned} & \text { 苍 } \\ & \text { y } \\ & 0 \stackrel{0}{0} \\ & \text { Z } \end{aligned}$ | $\begin{aligned} & \text { 訁ِ } \\ & \stackrel{0}{2} \end{aligned}$ |  |  |  |
| 这 | N | $\cdots$ | さ | $\therefore$ | $\stackrel{\square}{2}$ | N | $\stackrel{\infty}{\sim}$ | $\stackrel{1}{2}$ | $\infty$ | $\bar{\infty}$ | ® | $\infty$ | $\pm$ | $\infty$ | $\infty$ | $\stackrel{\infty}{\infty}$ | $\infty$ | ¢ | 8 | Ј | \％ | ๙ | す | に |


| $\begin{gathered} \text { Item } \\ \text { Number } \end{gathered}$ | Name | Qty | Material | Body Type | $\begin{gathered} \begin{array}{c} \text { Mass } \\ (\mathbf{g}) \\ (\text { total }) \end{array} \\ \hline \end{gathered}$ | Diameter / Width (mm) | Length (mm) | Height (mm) | High Temp | Melting Temp $\left(\mathrm{F}^{\circ}\right)$ | Survivability |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 96 | Thrust Washer | 12 | AISI 316 Stainless Steel | Cylinder | 1.6164 | 6.1000 | 6.1000 | 0.8600 | No | - | Demise |
| 97 | Extractor Grid | 1 | $\begin{gathered} \text { AISI } 316 \text { Stainless } \\ \text { Steel } \\ \hline \end{gathered}$ | Plate | 19.900 | 31.876 | 2.5400 | 31.876 | Yes | $2550^{\circ}$ | Demise ( 76.0 km ) |
| 98 | Thruster Heatsink | 1 | $\begin{gathered} \hline \text { AISI } 316 \text { Stainless } \\ \text { Steel } \\ \hline \end{gathered}$ | Plate | 29.950 | 31.876 | 9.9060 | 31.876 | Yes | $2550^{\circ}$ | Demise ( 75.7 km ) |
| 100 | 1/8" Connector Tube | 1 | $\begin{gathered} \text { AISI } 316 \text { Stainless } \\ \text { Steel } \end{gathered}$ | Cylinder | 1.4976 | 3.1750 | 3.1750 | 29.322 | Yes | $2550{ }^{\circ}$ | Demise (77.4 km) |
| 101 | 1/8" 90deg Connector | 1 | $\begin{gathered} \hline \text { AISI } 316 \text { Stainless } \\ \text { Steel } \end{gathered}$ | Cylinder | 4.5199 | 3.1750 | 3.1750 | 59.082 | Yes | $2550^{\circ}$ | Demise (77.1 km) |
| 102 | Solenoid Valve | 4 | 316 Stainless Steel Chrome Core 18 | Cylinder | 22.707 | 6.3500 | 6.3500 | 51.950 | Yes | $2550{ }^{\circ}$ | Demise ( 77.1 km ) |
| 103 | 1/8" 10-32 Male SAE | 1 | $\begin{gathered} \text { AISI } 316 \text { Stainless } \\ \text { Steel } \\ \hline \end{gathered}$ | Cylinder | 13.409 | 15.127 | 15.127 | 24.892 | Yes | $2550{ }^{\circ}$ | Demise ( 75.9 km ) |
| 104 | 1/4" 10-32 Male SAE | 1 | AISI 316 Stainless Steel | Cylinder | 20.567 | 18.440 | 18.440 | 27.432 | Yes | $2550^{\circ}$ | Demise ( 75.5 km ) |
| 105 | 1/8" to 1/16" Port Connector | 1 | AISI 316 Stainless Steel | Cylinder | 1.1970 | 6.0960 | 6.0960 | 18.288 | Yes | $2550^{\circ}$ | Demise ( 77.5 km ) |
| 106 | 10-32 Female Adapter | 2 | $\begin{gathered} \hline \text { AISI } 316 \text { Stainless } \\ \text { Steel } \\ \hline \end{gathered}$ | Cylinder | 19.372 | 10.999 | 10.999 | 19.050 | Yes | $2550{ }^{\circ}$ | Demise ( 75.6 km ) |
| 107 | Union $1 / 8^{\prime \prime}$ to $1 / 16^{\prime \prime}$ | 1 | Stainless Steel 316 | Cylinder | 17.719 | 12.905 | 12.905 | 30.988 | Yes | $2550^{\circ}$ | Demise ( 75.4 km ) |
| 108 | 1/8" Connector Tube | 1 | Stainless Steel 316 | Cylinder | 1.8791 | 3.1750 | 3.1750 | 39.528 | Yes | $2550^{\circ}$ | Demise ( 77.4 km ) |
| 109 | 1/8" Connector Tube | 3 | Stainless Steel 316 | Cylinder | 3.6342 | 3.1750 | 3.1750 | 25.400 | Yes | $2550^{\circ}$ | Demise ( 77.3 km ) |
| 110 | $1 / 8^{\prime \prime}$ to $1 / 16^{\prime \prime}$ Port Reducing | 1 | AISI 316 Stainless Steel | Cylinder | 1.1970 | 6.0960 | 6.0960 | 18.288 | Yes | $2550^{\circ}$ | Demise ( 77.5 km ) |
| 111 | 1/4" Tube | 1 | AISI 316 Stainless Steel | Cylinder | 26.964 | 6.3500 | 6.3500 | 76.750 | Yes | $2550^{\circ}$ | Demise ( 75.8 km ) |
| 112 | 1/4", $1 / 8$ " Tee Fitting | 1 | $\begin{aligned} & \text { AISI } 316 \text { Stainless } \\ & \text { Steel } \end{aligned}$ | Box | 59.918 | 53.340 | 14.288 | 111.87 | Yes | $2550^{\circ}$ | Demise (76.9 km) |
| 113 | 1/2" to 1/4" Stem Reducer | 1 | AISI 316 Stainless Steel | Cylinder | 65.852 | 25.810 | 25.810 | 44.958 | Yes | $2550^{\circ}$ | Demise ( 74.0 km ) |
| 114 | 1/8" Tube | 1 | AISI 316 Stainless Steel | Cylinder | 1.8387 | 3.1750 | 3.1750 | 36.000 | Yes | $2550{ }^{\circ}$ | Demise ( 77.3 km ) |
| 115 | $1 / 8$ " to $1 / 16^{\prime \prime}$ Union Reducer | 1 | Stainless Steel 316 | Cylinder | 17.719 | 12.905 | 12.905 | 30.988 | Yes | $2550^{\circ}$ | Demise ( 75.4 km ) |
| 116 | 1/8" Tube | 1 | AISI 316 Stainless Steel | Cylinder | 2.1707 | 3.1750 | 3.1750 | 42.500 | Yes | $2550^{\circ}$ | Demise ( 77.3 km ) |
| 117 | 1/8" 180 deg Tube | 2 | $\begin{gathered} \text { AISI } 316 \text { Stainless } \\ \text { Steel } \end{gathered}$ | Cylinder | 8.3648 | 3.1750 | 3.1750 | 31.750 | Yes | $2550{ }^{\circ}$ | Demise ( 77.2 km ) |
| 118 | 1/8" Tee Fitting | 3 | Stainless Steel 316 | Box | 125.43 | 44.704 | 11.176 | 27.115 | Yes | $2550^{\circ}$ | Demise ( 75.6 km ) |


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| 害 | $\stackrel{\sim}{\sim}$ | $\stackrel{\varnothing}{\varnothing}$ | $\stackrel{\varnothing}{\varnothing}$ | $\stackrel{\sim}{\circ}$ | $\stackrel{\infty}{\infty}$ | $\stackrel{\overbrace{}}{\bullet}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\pi}{\sim}$ | $\stackrel{\overbrace{}}{\gtrless}$ | \％ |
|  | $\begin{aligned} & \stackrel{\rightharpoonup}{\infty} \\ & \underset{寸}{\infty} \end{aligned}$ | $\begin{aligned} & \dot{+} \\ & \substack{\infty \\ \dot{q}} \end{aligned}$ | $\begin{aligned} & \text { 几 } \\ & \infty \\ & \infty \\ & \infty \\ & \infty \end{aligned}$ | $\begin{aligned} & 0 \\ & \underset{\sim}{n} \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & \text { ì } \\ & \text { in } \end{aligned}$ | $\begin{gathered} \infty \\ \stackrel{\infty}{6} \\ \text { in } \end{gathered}$ | $\begin{aligned} & 8 \\ & 8 \\ & 8 \\ & 8 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { İ } \\ & \underset{\sim}{4} \end{aligned}$ | $\begin{gathered} \text { O} \\ \stackrel{\rightharpoonup}{2} \end{gathered}$ |  |
|  | $\begin{aligned} & \text { O} \\ & \stackrel{\circ}{=} \end{aligned}$ |  | $\stackrel{\circ}{\vdots}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{1} \\ & \underset{\sim}{n} \end{aligned}$ | $\frac{\mathrm{t}}{\frac{1}{6}}$ | $\frac{\text { d }}{\substack{\text { an }}}$ | $\begin{aligned} & \mathrm{B} \\ & \underset{\mathrm{I}}{ } \end{aligned}$ | $\begin{aligned} & 0 \\ & \infty \\ & \dot{\sim} \end{aligned}$ | $\begin{gathered} \underset{\sim}{\underset{\sim}{n}} \\ \underset{\sim}{n} \end{gathered}$ |  |
|  |  | No | $\begin{aligned} & \stackrel{\leftrightarrow}{\infty} \\ & \infty \\ & \infty \\ & \infty \end{aligned}$ | $\begin{aligned} & \underset{\sim}{c} \\ & \underset{\sim}{c} \end{aligned}$ | $\begin{aligned} & \frac{4}{6} \\ & \stackrel{3}{9} \end{aligned}$ | $\begin{gathered} \text { d } \\ \stackrel{\rightharpoonup}{\mathbf{o}} \end{gathered}$ | $\begin{aligned} & 8 \\ & \vdots \\ & \mathrm{I} \end{aligned}$ | $\begin{aligned} & 0 \\ & \infty \\ & \underset{\sim}{\infty} \end{aligned}$ |  |  |
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|  |  | $\begin{aligned} & \stackrel{\rightharpoonup}{\stackrel{\pi}{0}} \\ & \underset{\sim}{E} \end{aligned}$ | － | 会 |  |  |  |  | $\begin{aligned} & \stackrel{\rightharpoonup}{\stackrel{\rightharpoonup}{0}} \\ & \stackrel{F}{E} \end{aligned}$ |  |
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|  |  |  |  | $\begin{aligned} & 3 \\ & 0 \\ & 0 \\ & 0 \\ & \vdots \\ & \vdots \\ & \vdots \end{aligned}$ | $1 / 16^{\prime \prime}$ to $1 / 8^{\prime \prime}$ Stem Adapter |  |  |  |  |  |
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