



***Reentry Risk Assessment for Spaceflight
Inc Sherpa-LCT1***

***Dr. Michael A. Weaver
Fluid Mechanics Department***

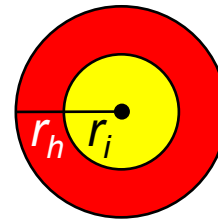
24 February 2022



Reentry Risk Assessment Process

- Casualty risk or **expected casualties (E_C)** depends on:
 - *Size and number of objects that impact the surface*
 - *Human population within geographic debris impact region*
- Method for determining casualty expectation:
 - *Find vehicle **debris area** that survives reentry (survivability analysis)*
 - Depends on component characteristics and flight trajectory
 - “Risky” objects: shielded from heating and/or high melt/ablation temperature
 - *Calculate **casualty area (A_C)** – area of interaction between tumbling debris objects and an average human:*

$$A_C = \sum_{i=1}^N \left(\sqrt{\pi r_h^2} + \sqrt{\pi r_i^2} \right)^2$$



r_h = human radius = 0.34 m

r_i = radius for i^{th} object of N total

Applies when kinetic energy > 15 J

- *Find **population at risk (ρ)** within debris impact region*
 - For random reentry, impact region is bounded by North/South latitudes corresponding to orbital inclination, and population at risk is latitude-weighted
 - Expressed in terms of expected casualties per casualty area
- *Calculate **expected casualties: $E_C = \rho A_C$***



Modeling Reentry Survivability

- Flight Trajectory
 - *Rigid-body dynamics*
 - *Planet (Earth) dynamics*
 - *Atmosphere model and drag bridging*
 - *Gives velocity, altitude, flight path angle, deceleration*
- Heating Environment
 - *Free-molecular heating and continuum aeroheating*
 - *Transition bridging between free-molecular and continuum regimes*
 - *Gives heat transfer coefficient over the surface*
- Body Response
 - *Transient conduction with re-radiation cooling*
 - *Wall phase change (melting or ablation)*
 - *Gives wall temperature and mass change*



AHaB Reentry Survivability Tool

- AHaB (Atmospheric Heating and Breakup) developed under Aerospace IR&D
- Flight Trajectory Approach
 - *3-DOF rigid-body dynamics*
 - *Oblate, rotating Earth*
 - *4th-degree zonal harmonics*
 - *Martino model for drag bridging*
 - *1976 US Standard Atmosphere*
 - *Can also read pre-defined trajectories*
- Heating Environment Approach
 - *Free-molecular heating*
 - Expression for impact normal to flat plate, with shape factors (based on methods of Cropp and Klett, Sandia)
 - Function of density and velocity ($\propto \rho, V^3$)
 - *Continuum aeroheating*
 - Detra-Kemp-Riddell correlation for stagnation point, with shape factors (based on methods of Cropp and Klett, Sandia)
 - Function of body radius, wall temperature, freestream velocity, freestream density ($\propto 1/\sqrt{R}, \sqrt{\rho}, V^{3.15}$)
 - *Transition bridging*
 - Matting model (NASA) between free-molecular and continuum regimes

AHaB Reentry Survivability Tool



- Heating Environment Approach, cont'd
 - *Additional models available, as needed*
 - Oxidation heating – proper use requires configuration-dependent and time-dependent empirical data
 - Radiative heating using Tauber-Sutton approach for super-orbital airspeeds
- Body Response Approach
 - *Transient conduction*
 - 1-D conduction equation generalized to Cartesian, cylindrical, and spherical coordinates
 - Implicit finite-volume discretization for unconditional numerical stability
 - Flexible boundary conditions (heat flux or temperature, as needed)
 - *Re-radiation cooling*
 - Stefan-Boltzmann law for gray bodies
 - *Wall phase change (melting or ablation)*
 - Wall temperatures will not exceed material melt/ablation temperature
 - Mass removed from external surface according to applied heat of fusion
 - Conduction continues through wall
 - Mass loss ceases if temperature falls below melt/ablation temperature



Survivability Analysis Approach with AHaB

- Initial trajectory:
 - *Spacecraft assumed to be tumbling*
 - *Orbital decay simulated from initial orbit to 120 km altitude (entry interface)*
 - *Survivability analysis initialized at entry interface*
- Component separation and demise (complete mass loss) assumptions:
 - *All components are initially attached to spacecraft*
 - *Demise may occur for either attached or separated components*
 - *Demise or initial melting may release attached components, depending on details of specific attachment configuration*
 - *Components may be thermally shielded by other components*
- Survivability is modeled with AHaB tool, providing:
 - *Sequence of events for reentry breakup*
 - *Debris separation altitudes from parent body*
 - *Debris demise altitudes*
 - *Mass, debris area, and casualty area of surviving debris*



Data Needed for Survivability Analysis

- Detailed analysis approach requires the following:
 1. *A parts list for spacecraft ("parts" includes housing contents, where applicable, e.g., battery cells, reaction wheels, etc.)*
 2. *Masses for each part (e.g., mass statement)*
 3. *Material for each part (e.g., Al 2024, 410 SS, CRES, Ti-6Al-4V, etc.)*
 4. *Physical dimensions for each part (height, width, length, wall thickness, facesheet thickness, honeycomb density, etc.)*
 5. *Briefing charts, schematics, and drawings illustrating shape of each part (charts often suffice)*
 6. *Briefing charts, schematics, and drawings showing placement of parts in relation to each other (charts often suffice)*
 7. *Initial parameters of the disposal orbit (orbital inclination, at a minimum)*
 8. *Expected year of reentry (a.k.a., orbital lifetime)*



Data Sources and Assessment Conditions

- Component and configuration data derived from Spaceflight Inc:
 - “*Sherpa-LTC Summary for Aerospace Corp.pdf*,” 29 Sep 2021
 - “*Sherpa-LTC Summary for Aerospace Corp Benchmark.pdf*,” 28 Jan 2022
 - “*Sherpa-LTC ODAR Analysis.xlsx*,” 28 Jan 2022
 - “*Sherpa-LTC Inputs to Aerospace Corp 20220214.xlsx*,” 14 Feb 2022
 - “*RE: [External] - RE: DAS input file for Sherpa-LTC1*,” 22 Feb 2022, email with data for revised propellant tanks replacing steel alloy with aluminum alloy
 - “*RE: [External] - RE: DAS input file for Sherpa-LTC1*,” 24 Feb 2022, email with expected year of reentry
 - Point of contact: Eric Lund (elund@spaceflight.com)
- Assessment conditions:
 - *Reentry in year 2025*
 - *53° orbital inclination, with confirmation to 97.7° (Sun-synchronous) inclination*
 - *Circularization through natural decay simulated to 120 km*
 - Trajectory initial conditions for analysis are those at 120 km
 - *Initial temperature of 300 K at 120 km*

Survivability Results

53° Orbital Inclination



Time (E+)	Key Events	Demise	Notes
1071 sec	88.2 km	CCS & 2-way QuadPack	Property estimated, or dimension derived from mass
1100 sec	85.6 km	RZA & 4-way QuadPack	Survives and poses risk
1208 sec	70.6 km	24-inch J-channel spacer ring	Risk negligible or KE < 15 J
1221 sec	68.0 km	CAB hex plate	
1255 sec	59.9 km	Aft CAB Bulkhead	

Object Description	Shape	Count	Material Type	Diam/Width (m)	Length (m)	Wall/Core Thickness (m)	Face Sheet Thickness (m)	Height or Min Diam (m)	Unit Mass (kg)	Total Mass (kg)	Separation Altitude (km)	Demise Altitude (km)	Debris Area (m ²)	Total Debris Area (m ²)	Total Casualty Area (m ²)
STRUCTURE AND EQUIPMENT															
Upper half of 24-in separation system	Ring	1	Al 6061-T6	0.610	0.031	0.011			1.80	1.80		84.2	0.000	0.000	0.000
24-inch J-channel spacer ring	Ring	1	Al 6061-T6	0.667	0.083	0.011			5.26	5.26		70.7	0.000	0.000	0.000
Solar panel wing	Plate	6	Al 6061-T6	0.546	0.549	0.003		0.060	2.35	14.10		96.0	0.000	0.000	0.000
CAB hex plate	Ring	2	Al 6061-T6	0.822	0.070	0.021			10.00	20.00		68.0	0.000	0.000	0.000
CAB interior wall	Plate	6	Al 6061-T6	0.118	0.318	0.008			0.83	4.98	68.0	67.8	0.000	0.000	0.000
CAB corner brace	Box	6	Al 6061-T6	0.151	0.178	0.004		0.151	1.10	6.60		88.2	0.000	0.000	0.000
Port 4 avionics adapter plate	Plate	1	Al 6061-T6	0.294	0.311	0.005			1.15	1.15		71.9	0.000	0.000	0.000
RZA-Core	Box	1	Al 6061-T6	0.285	0.285	0.005		0.090	3.20	3.20		85.6	0.000	0.000	0.000
NSL black box std	Box	1	Al (generic)	0.054	0.089	0.006		0.047	0.29	0.29		83.0	0.000	0.000	0.000
Camera bracket	Plate	2	Al 6061-T6	0.146	0.178	0.006			0.62	1.24		85.6	0.000	0.000	0.000
IMPERX camera	Box	2	Al 6061-T6	0.037	0.072	0.004		0.037	0.12	0.23		88.2	0.000	0.000	0.000
Camera lens assembly	Cylinder	2	SS 304	0.034	0.047	0.003			0.13	0.27	85.6	73.3	0.000	0.000	0.000
Battery thermal isolator	Plate	2	G10/FR4	0.102	0.145	0.009			0.26	0.52		70.6	68.6	0.000	0.000
Battery module	Box	2	Al 6061-T6	0.100	0.139	0.018		0.100	2.65	5.30	68.6	58.1	0.000	0.000	0.000
QuadPack adapter plate	Plate	4	Al 6061-T6	0.297	0.311	0.007			1.73	6.91		68.8	0.000	0.000	0.000
Empty 2-way QuadPack	Box	2	Al 6061-T6	0.250	0.440	0.004		0.250	6.30	12.60		88.2	0.000	0.000	0.000
Empty 4-way QuadPack	Box	1	Al 6061-T6	0.250	0.440	0.005		0.250	7.50	7.50		85.6	0.000	0.000	0.000
QuadPack mass model	Box	1	Al 6061-T6	0.250	0.528	0.017		0.250	26.30	26.30	68.0	64.4	0.000	0.000	0.000
RPG base ring	Ring	1	Al 6061-T6	0.626	0.038	0.026			5.08	5.08	68.0	54.8	0.000	0.000	0.000
RPG leg	Box	6	Al 6061-T6	0.051	0.196	0.006		0.051	6.30	37.8	54.8	54.2	0.000	0.000	0.000
RPG triangle plate	Plate	1	Al 6061-T6	0.346	0.400	0.012		0.076	4.47	4.47		69.2	0.000	0.000	0.000
RPG MLB adapter plate	Plate	3	Al 6061-T6	0.255	0.322	0.027			2.43	7.29	54.2	53.2	0.000	0.000	0.000
Lower 8-in separation system	Ring	3	Al 6061-T6	0.118	0.045	0.039			1.19	3.57		53.9	0.000	0.000	0.000
CCS enclosure	Box	1	Al 6061-T6	0.190	0.382	0.004		0.272	4.81	4.81		88.2	0.000	0.000	0.000
Torque rod	Cylinder	3	Iron	0.020	0.300	0.004			0.45	1.35	88.2	67.0	0.000	0.000	0.000
AD avionics	Box	4	Al 6061-T6	0.120	0.150	0.016		0.100	3.00	12.00	88.2	66.1	0.000	0.000	0.000
RWA enclosure	Box	3	Al 6061-T6	0.140	0.150	0.003		0.042	0.57	1.71	88.2	80.6	0.000	0.000	0.000
RWA rotor	Ring	3	SS 410	0.135	0.037	0.003			0.40	1.20	80.6	69.7	0.000	0.000	0.000
PROPULSION															
100504 AFT CAB BULKHEAD	Disk	1	Al 7076-T6	0.572		0.025			3.32	3.32	70.6	59.9	0.000	0.000	0.000
100602 DMLS PRESSURANT TANK POLARIS 100417 CONFIG	Cylinder	2	Ti-6Al-4V	0.085	0.327	0.003			0.98	1.96	59.9	0.0	0.028	0.056	1.176
100535 OX TANK ASSEMBLIES	Cylinder	3	Al 6061-T6	0.204	0.340	0.004			4.75	14.25		64.1	0.000	0.000	0.000
FLUID COMPONENTS, TOP HALF	Cylinder	1	SS 316	0.025	0.416	0.0125			3.27	3.27		62.3	0.000	0.000	0.000
100733 FUEL TANK ASSEMBLY	Cylinder	1	Al 6061-T6	0.204	0.340	0.004			4.75	4.75		88.2	0.000	0.000	0.000
100719 A LEG, THRUST DECK	Beam	3	Al 7076-T6	0.015	0.243	0.004		0.015	0.22	0.66		89.6	0.000	0.000	0.000
FLUID COMPONENTS, BOTTOM HALF	Cylinder	1	SS 316	0.025	0.387	0.0125			3.60	3.60		74.0	0.000	0.000	0.000
100716 THRUST BULKHEAD, POLARIS	Ring	1	Al 7076-T6	0.446	0.013	0.021			1.03	1.03		82.8	0.000	0.000	0.000
100688 OCELOT ENGINE ASSEMBLIES	Cylinder	4	Niobium-C103	0.086	0.202				0.51	2.04	82.8	0.0	0.017	0.069	2.141
Totals		88								154.34				0.1	3.32

88.6 kg were part of analyzed configuration but not part of Sherpa-LTC2

RWA rotors

Titanium tanks

Fluid comps, top

Fluid comps, bottom

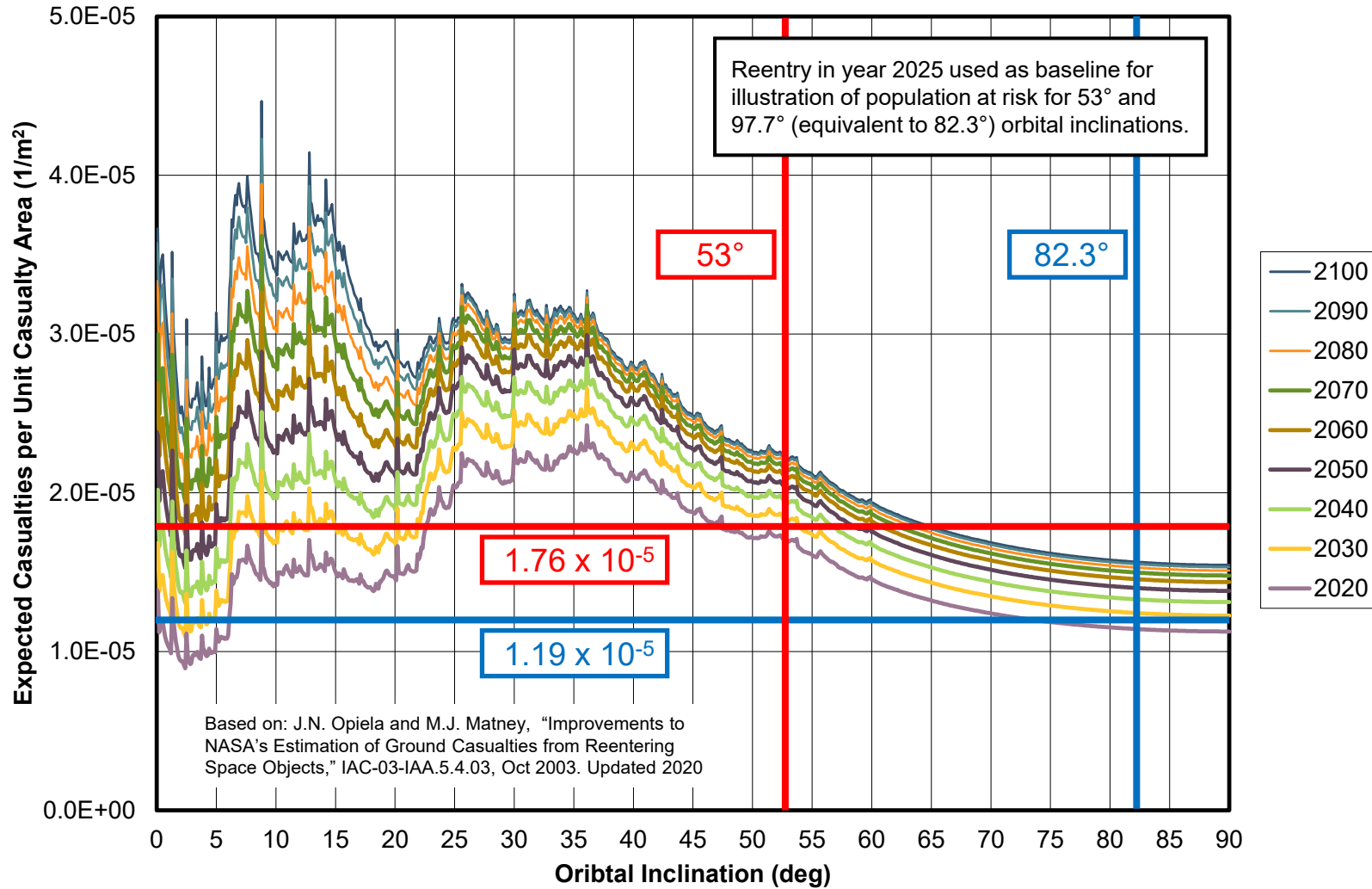
Ocelot engines

Casualty Area



Object Name	Material	53° Inclination		97.7° Inclination	
		Part Count	Casualty Area (m ²)	Part Count	Casualty Area (m ²)
Pressurant Tank	Ti-6Al-4V	2	1.176	2	1.176
Engine	Niobium-C103	4	2.141	4	2.141
TOTAL		6	3.32	6	3.32

Population at Risk





Expected Casualties

- For reentry in year 2025, predicted expected casualties for 53° inclination are:

$$(3.32 \text{ m}^2) \times (1.76 \times 10^{-5} \text{ m}^{-2}) = 0.6 \times 10^{-4}$$

- For reentry in year 2025, predicted expected casualties for 97.7° inclination are:

$$(3.32 \text{ m}^2) \times (1.19 \times 10^{-5} \text{ m}^{-2}) = 0.4 \times 10^{-4}$$

- US Government Orbital Debris Mitigation Standard Practices (ODMSP) specify that expected casualties from reentry be less than 1×10^{-4}

- Notes on reported results:

- *Items denoted as “Risk negligible or $KE < 15 \text{ J}$ ” are either made from materials with no risk of surviving or have less than 15 J of kinetic energy at ground impact, or both, and do not pose a casualty risk*
- *Results are subject to revision based on receipt of additional and/or modified data*

- On the next chart, expected casualties are parameterized for future years over the orbital-inclination range of interest

Expected Casualties

